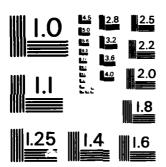
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Umweltforschung

Kreuzeckbahnstraße 19

D-8100 Garmisch-Partenkirchen Telefon 0 88 21 / 5 10 56-57

Institutsleitung: Dr. Reinhold Reiter

Title of the Research Project:

VISIBILITY AND VERTICAL STRUCTURE MEASUREMENTS IN SOUTHERN GERMANY

Principal Investigator:

Dr. Reinhold Reiter, Director

Name of Contractor:

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Short Description of the Lidar System Used for this Research, Improvements and Modifications

The lidar used for this project is a mobile system with a ruby and a neodymium glass laser transmitter. Both lasers are operated with and without frequency doubling, resulting in available frequencies of 347, 530, 694, and 1060 nm. The backscattered light is collected by a 30 cm dia. reflecting telescope, and detected by an EMI 9813 photomultiplier tube with bialkali cathode (347 and 530 nm) and a large-area PINdiode with broadband amplifier (694 and 1060 nm). The signals are digitized by a Biomation 8100 transient recorder with 8 bit amplitude resolution, 10 ns minimum sample interval and 2000 bytes memory, and further processed by an on-line computer. The range-corrected and energy-normalized backscatter profiles are represented on a display tube and plotted by an X-Y plotter, both incorporated in the lidar system. The digitized original returns are stored on floppy disks or magnetic tape cassette, together with housekeeping and other auxiliary data. Z ...

In the past, the change from the fundamental wavelength to the first harmonic was done for both lasers through manual replacement of the beam expanding telescopes which are focused and aligned respectively for only one wavelength. The frequency doublers were connected to one of the telescopes each. In order to avoid this time-consuming procedure, at least for the neodymium laser, an achromatic telescope with common focus for 530 and 1060 has been calculated and constructed, which can remain permanently in the beam path, so that the neodymium laser transmits both wavelengths simultaneously. The time lag between measurement in both wavelengths is thus only limited by the data processing time, which is a few seconds if a real-time display and plot of the normalized profiles is dispensed with.

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Unfortunately, a similar procedure is not applicable to the ruby laser because no UV-permeable optical glasses with sufficiently different dispersion are available. For the present task the 347 nm wavelength is less important anyway. Nevertheless, an optical construction is in progress allowing the expanding of the 694 nm beam by the new achromatic telescope, too. For this purpose, a beam divider and a deflection mirror will be built into the system.

The originally fixed gain of the diode detector amplifier proved to be too high for the recording of the strong back-scatter signals from clouds and fog without overload effects. For attenuation of those signals two neutral filters with transmissivities of 50 and 25%, respectively, were inserted into free positions of the interference wheel. Furthermore, by switching to a smaller feedback resistor, it is now possible to reduce the gain by a factor of 11.6.

2. Program Developments

The application of Klett's evaluation method for lidar returns requires a considerable amount of computation work. To do this, some time ago a program was developed for the lidar on-line computer. Profiles of the extinction coefficient calculated from the lidar data by Klett's method and the "standard" method, where the boundary value is chosen close to the lidar system and the integration of the lidar equation proceeds away from it (called "CRBV method" in the previous interim report), were plotted by the above-mentioned X-Y-plotter. This plotter, however, is not very comfortable and precise, especially if curves with heavy fluctuations are to be displayed. Furthermore, the memory capacity of the lidar on-line computer (32 k bytes) is somewhat too small for the handling of large amounts of data like digitized lidar returns. For these reasons

we decided to transfer all raw lidar data via magnetic tape to the larger computer which is available since about a year. This computer offers 512 k RAM and 400 megabytes disc memory. The operating system can support up to 63 simultaneous users. Each user is totally independent and has 768 kilobytes virtual memory at his disposal. An extensive library of auxiliary programs and subroutines is available, for instance, routines for the precise display of curves on a graphic terminal screen or by an incremental plotter.

The programs for the application of the Klett and standard method for the evaluation of lidar returns have been rewritten in FORTRAN language for this new computer. Furthermore, extensions have been made for performing the following tasks:

- listing of the digitized original lidar return as function of distance
- linear plot of the original, not range-corrected lidar return
- linear plot of the range-corrected lidar profile in absolute units
- logarithmic plot of the range-corrected lidar profile,
- linear plot of the extinction coefficients and optical depth profiles, calculated by the standard and Klett's method
- listing of the extinction coefficient and optical depth versus distance
- storage of digitized raw lidar data and calculated extinction coefficient and optical depth profiles on magnetic tape in any desired format.

The disc memory capacity of the computer is large enough for permanent storage of numerous lidar returns and calculated profiles of optical parameters, which greatly facilitates the computation work. Examples of listed and plotted profiles will be described in Chapter 4.

3. Measurements

In general, situations with strong and inhomogeneous fog or aerosol backscatter in the near-ground atmosphere occur less frequently during summertime. However, in some cases we were able to get lidar returns from a turbid atmosphere, with scattering coefficients distributed both homogeneously and inhomogeneously along the laser beam path (measurements before April 1983 have already been listed in the previous interim reports).

On <u>June 29</u>, a very humid air mass with high aerosol concentration was present, and in the morning some low-level cumulus fractus clouds occurred. Spatial inhomogeneities of the backscatter coefficient were observed also outside the cloud, caused by partial precondensation (growth of the aerosol particles due to water absorption). Towards noon, the humidity decreased, and the backscatter became homogeneous in the lowest 1000 m of the atmosphere. Five measurement series were obtained in the wavelengths 530, 694, and 1060 nm.

On <u>July 14</u>, similar aerosol conditions occurred after a thunder-shower. Again, cumulus fractus clouds were observed about 400 m above ground level during the morning hours, and strong and initially inhomogeneous aerosol backscatter below. Like on June 29, the backscatter homogenized with decreasing humidity towards noon time, but the concentration of the dry aerosol was considerably higher in this case. Eleven series of measurements were performed in each wavelength. One of them will be discussed in more detail in the next section of this report.

During the next day, <u>July 15</u>, the aerosol constitution remained nearly unchanged. In the afternoon some measurements were performed under homogeneous conditions.

On <u>August 12</u>, a shallow layer of low-concentrated ground fog was present during the late night and early morning hours. This layer, however, dissolved then very rapidly, and so only one lidar return was obtained at 6 AM CET.

4. Further Example of Extinction Coefficient Profiles Calculated by the Klett and CRBV Method, Application of Aerosol Data for Derivation of Klett Boundary Values

The basic principle of Klett's method is to choose the boundary value for the extinction coefficient at the far end of the range interval, not at the close one. The dependence of this boundary value (BV) upon the resulting extinction coefficient profile is the less the higher the optical depth is at that point. In the previous interim report from 21 March we pointed out that under dry aerosol conditions, even at extremely high concentrations, the optical depth at a 3 km range is in most cases not high enough to keep the influence of the BV sufficiently low. Increasing the lidar range is not always applicable due to the signal-to-noise ratio, rapidly increasing with distance. In such cases, therefore, a BV more or less close to reality must be found. If the spatial aerosol distribution is sufficiently homogeneous, the slope or average slope of the rangecorrected backscatter profile may be used for this purpose. In our case, we have the advantage to operate an unmanned measuring station for meteorological and aerosol data at a mountain peak at 1650 m altitude above MSL, 2.55 km apart from the Institute, in connection with an atmospheric transmission path. The station can be switched on and off by a radio signal. Aerosol size distributions are measured by a Knollenberg classical scattering aerosol spectrometer, Model PDS-200. From the measured particle size spectra, extinction coefficients as a function of wavelength can be calculated using van de Hulst's approximation formula. On July 14, the particle spectrometer was operated during the lidar measurements, and extinction coefficients were calculated for the lidar wavelengths. Fig. 1 presents an original lidar return in 694 nm (ruby laser) wavelength, normalized with respect to transient recorder input range and laser energy but not to range, i.e. the curve is proportional to the electrical signal from the photodetector

(the peak near the end of the range is the reflex from a mountain face). The profile was calculated by the new program mentioned in Chapter 2, displayed on a graphic terminal screen and hardcopied. At the upper left corner are given the profile identifier, composed of a two-digit series number, a wavelength code (A), and the date, and, below it, the maximum abscissa (range) and ordinate values. The ordinate units here are volts/Joule. A listing of the digitized profile amplitude as function of range in meters is presented in Table 1 in the appendix. In this table the data proceed linewise (horizontally) with distance. Each line contains six pairs of distance (in m) and amplitude values; the amplitudes in this case are the digital numbers delivered by the transient recorder (or the sum of them, if more than one signal is averaged) minus the background level, without any normalization factor. The format of the lines is described by the FORTRAN-statement FORMAT(6(F7.1,I5)). In this presentation mode the limited amplitude resolution of the signal digitizer remains clearly evident. The whole table is stored as a data file in the disc memory of the computer in the same format, i.e. one line with six data pairs is one record. The transfer to other carriers, e.g. magnetic tape, is thus very simple by calling a special service program. The example is a lidar return from a homogeneous atmosphere; a return from an inhomogeneous cloud is listed in Table 2, it is the example discussed in the 1st interim report from February 10, 1983.

Fig. 2 shows the range corrected backscatter profile calculated from the lidar return Fig. 1; since calibration factors are known for each wavelength, the profile amplitude, presenting the product $\theta \cdot \tau^2$ (θ =backscatter coefficient, τ =transmissivity factor), can be given in absolute units, m^{-1} sterad⁻¹. In the upper left corner again are shown the identifier and the abscissa and ordinate maxima, XM and YM, respectively.

For some purposes a logarithmic plot of the range-corrected profile is desirable. In Fig. 3 our profile is presented in such a way, where the decadic logarithm has been chosen. The full ordinate range is one decade in linear scale or unity in logarithmic scale, as indicated in the upper left corner. The nearly linear decay of the lidar profile in this presentation indicated almost homogeneous aerosol conditions, and an average extinction coefficient .315 km⁻¹ is easily derived.

As already mentioned above, for our example we have aerosol concentration and size distribution data from the far end of the lidar range interval, which can be used for the derivation of the Klett boundary value. Fig. 4 shows hourly averaged particle size distribution curves measured near the end of the lidar range by an optical sprectrometer. The size range is .32 to 20 microns in diameter. From the spectrum closest to the time of the lidar measurement, van de Hulst's approximation results in an extinction coefficient of 1.57 km⁻¹ for the ruby wavelength, where a refractive index of 1.419-.03311 was assumed, according to Shettle & Fenn's urban aerosol model at a relative humidity of 80% as measured. If we use the extinction coefficient just mentioned and apply Klett's method to our lidar profile, we get the extinction coefficient profile shown by the solid curve in Fig. 5. The dashed line is the optical depth as function of range. Above left are given the file identifier as before, the maximum abscissa value (3000 $\ensuremath{\text{m}}$ in this case), the ordinate maxima for extinction coefficient (YMS) and the optical depth (YMT), the chosen value of the exponent Q in the exponential relation between backscatter and extinction coefficients (here: 1), the reference distance REFD, and the boundary value SR.

We see in Fig. 5 that the BV calculated from the measured aerosol data is obviously too high, as indicated by the unrealistic increase of the extinction coefficient towards the end

of the interval. Actually the sprectrometer-derived extinction is almost five times higher than the slope value. The reason for this discrepancy, which was observed in other cases, too, is not yet known. A local enhancement of particle size at the spectrometer site due to cloud formation or precondensation is improbable, since the measured relative humidity never exceeded 80%. Nevertheless, the extinction coefficient derived from aerosol data assessed at ground level is much smaller than that from the rear end of the lidar range interval, namely .185 km⁻¹, calculated from optical spectrometer data and .175 km⁻¹, calculated from impactor data. These values are even smaller than the extinction coefficient derived from the lidar profile slope. Further investigations seem to be required in the future to find the reason for these discrepancies.

If the Klett method is applied with the slope extinction coefficient as BV, the profile presented in Fig. 6 is obtained. As expected, a nearly constant extinction coefficient results. The same is true if the standard or CRBV method is applied with that boundary value at the near end of the interval, as shown in Fig. 7. The meaning of the solid and dashed curves is the same as before. Above left are printed the identifier, the close and far ends of the range interval, XR and XE, the coordinate maxima for range, extinction coefficient and optical depth, XM, YMS and YNT, respectively, the exponent Q, and the boundaryvalue SR, here valid for range XR.

A comparison of Figs. 6 and 7 suggests both methods to be equivalent for lidar returns from a homogeneous atmosphere. However, the Klett method is still superior in so far that the choice of the BV is much less critical.

The extinction and optical depth profiles obtained by the Klett and CRBV methods may be stored permanently as data files in the

disc memory of the computer. Since these files are very extensive, we present in the appendix, Table 3, only the beginning of such a file, here, the Klett profile shown in Fig. 5. The first line contains the maximum number of profile data points and the maximum extinction coefficient and optical depth, the second one the reference distance in m, the boundary value in m⁻¹, and the exponent Q. The lines following contain the range in m, the extinction coefficient in m⁻¹, and the optical depth.

5. Future Plans

The soft-ware is now complete except some improvements like plotting of coordinate scales in the diagrams. One of the tasks of this contract work is the examination of the appropriateness of the relationship

$$\beta(r) = a \cdot \sigma(r)^q$$
.

Only if this relationship is valid an analytical solution of the lidar equation exists. The examination of the validity is somewhat difficult. A possible way to do this is to correlate the absolute lidar amplitudes close to the lidar, where the extinction can be neglected, with extinction coefficients at the same range, calculated by any appropriate method. For this purpose as many as possible measurements are required, during fog and cloud conditions from within the fog. This is necessary to get absolute fog backscatter data. In order to get such data it will be necessary to go with the lidar to sites where ground fog is more frequent than at our Institute. Such places exist in the plains outside of our valley; e.g. in the "Murnauer Moor" or in other areas not too far from here. Since only a part of such excursions can be expected to be fully successful, it is doubtful that this task on the basis of experiments, data evaluation, and theoretical work can be finished during the current contract.

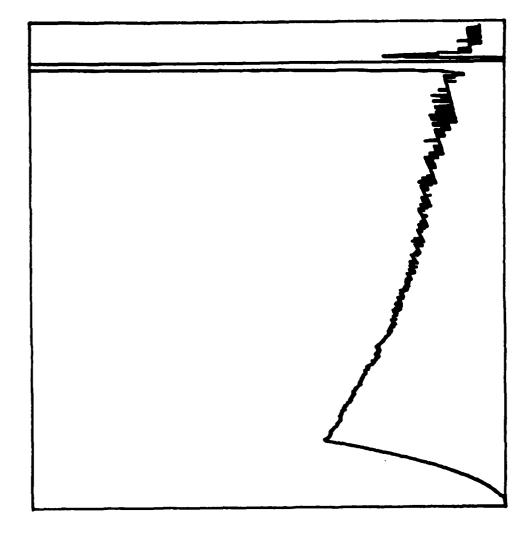
On the other hand, the lidar shots close to the aerosol spectrometer at the mountain station should be continued to find out whether a general discrepancy exists between spectrometer— and lidar—derived extinction coefficients.

Garmisch-Partenkirchen, September 8, 1983

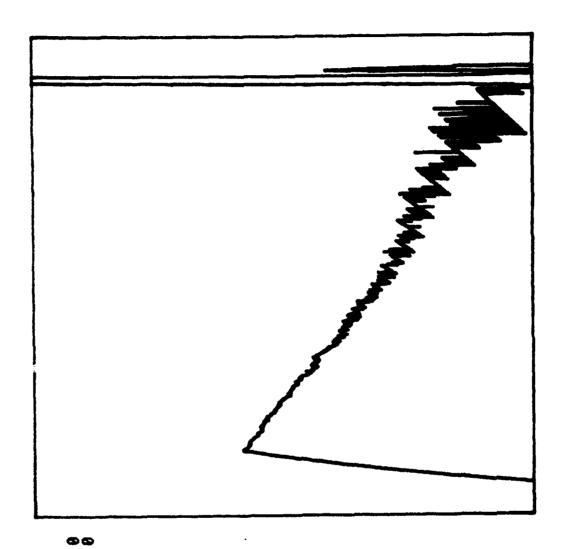
(Dr. R. Reiter)
Director

FIGURES 1-7

10A140783 XM=3000.0 H YM=0.5E 03 U/JOULE Fig.1

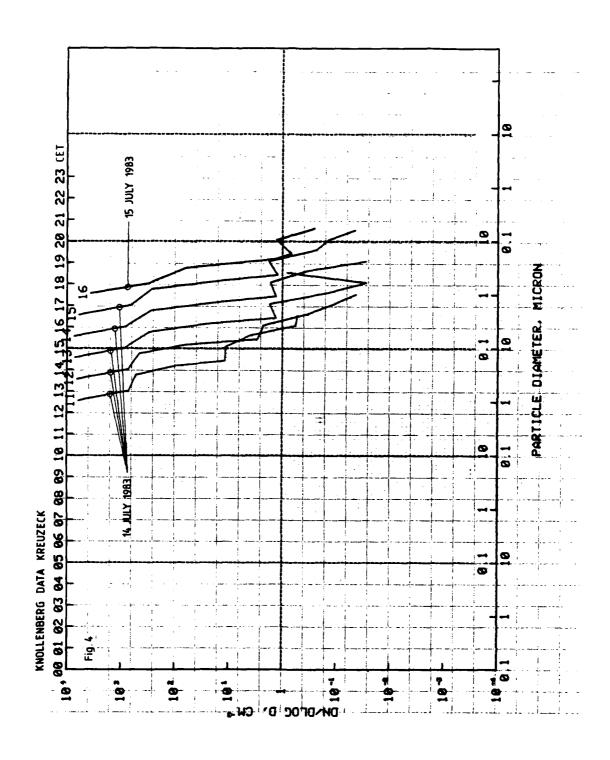


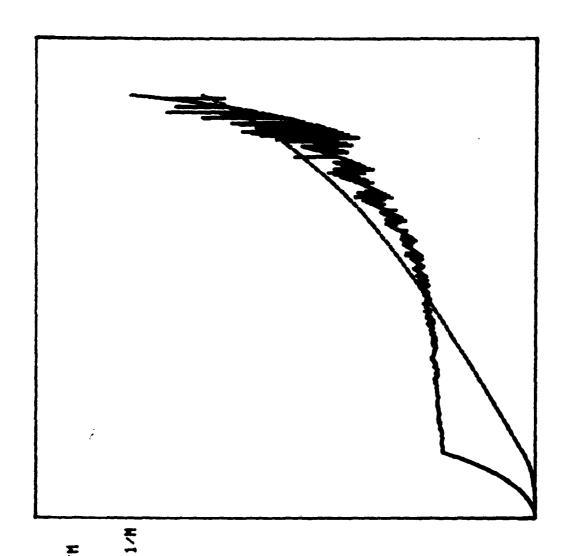
18A148783 XM=3888.8 M YM=8.1E-84 1/M Fig.2



186148783 XM=3068.0 H LOG18(YMIN)=-LOG18(YMRX)=-Fig.3

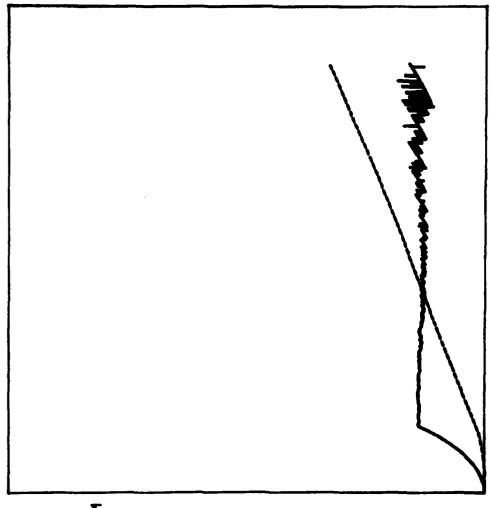
*..





104140783 XH=3000 0 M YMS=6.2E-02 YMT=6.2E-01 Q=0.1000E-01 REFD=2650 0 SR=0.1570E-01

F19.5



10A140783 XM=3000.0 M YMS=0.2E-02 1/M YMT=0.2E 01 Q=0.1000E 01 REFD=2650.0 M SR=0.3150E-03 1/M Fig.6

XR=2649.0 H XR=3600.0 H YNS=6.2E-02.1 YNT=0.2E-01 YNT=0.2E-01 SR=0.3150E-03 SR=0.3150E-03

APPENDIX

TABLES 1-3

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19.5	425	24.0	152	22.5	145	24.9	148	25.5	153	27.8	168
28.5	185	30.0	208	31.5	213	33.6	225	34.5	225	36.0	226
37.5	249	39.9	244	40.5	249	42.8	266	43.5	265	45.8	268
46.5	272	48.0	276	49.5	285	54.8	299	52.5	294	54.6	383
55.5	349	57.0	336	58.5	353	49.9	394	61.5	425	63.8	465
64.5	554	66.0	645	67.5	664	69.0	728	70.5	743	72.6	751
73.5	754	75.8	754	76.5	751	78.8	754	79.5	754	84.8	/54
82.5	254	84.0	754	85.5	751	87.8	75.1	88.5	754	98.6	75.4
91.5	754	93.0	754	94.5	754	96.0	754	97.5	754	99.0	754
100.5	251	102.0	754	103.5	754	165.6	754 754	166.5	75.1 20.4	168.6	751 751
189.5	754	414.9	754	112.5	754 754	114.8 123.8	751 751	115.5 124.5	754 754	147.0 126.0	751
118.5 127.5	254 254	420.6 429.8	754 754	424.5 43 0. 5	751	132.8	754	133.5	751	135.0	/51
136.5	754	138.0	751	139.5	751	144.0	751	142.5	751	144.8	75 1
145.5	754	147.8	754	148.5	754	159.8	754	151.5	754	453.8	754
154.5	751	156.0	751	157.5	751	159.0	254	160.5	751	162.0	754
163.5	754	165.0	751	166.5	754	168.8	754	169.5	754	171.8	751
172.5	75	174.0	751	175.5	751	177.0	754	178.5	251	182.0	751
484.5	751	183.0	754	184.5	754	486.8	754	187.5	754	187.8	754
190.5	254	192.0	751	193.5	754	195.8	754	196.5	754	498.6	754
199.5	754	201.0	754	202.5	751	204.0	754	205.5	751	297.8	751
208.5	754	218.0	75 f	211.5	754	213.0	754	244.5	254	246.0	754
247.5	751	249.0	754	220.5	754	SSS.8	754	223.5	754	225-8	751
226.5	754	228.0	754	229.5	754	231.0	751	232.5	754	234.0	754
235.5	751	237.8	751	238.5	754	249.8	754	241.5	754	243.8	751
244.5	751	246.0	754	247.5	251	249.8	754	250.5	251	252.6	754
283.5	754	255.9	754	256.5	751	288.8	751	259.5	751	264.8	754
262.5	254	264.6	751	265.5	751	267.0	754	268.5	754	270.0	754 754
2/1.5	754 754	273.9 282.0	751	274.5 283.5	754 754	276.0 285.0	754 754	277.5 286.5	754 754	279.0 288.6	751 751
280. 5 289.5	751	291.0	751 751	292.5	751	294.8	751	295.5	751	297-8	75 f
298.5	251	300.0	751	381.5	751	303.0	754	384.5	751	306.6	754
397.5	754	307.0	751	349.5	754	312.0	754	343.5	754	345.9	751
316.5	251	348.0	751	349.5	754	321.0	754	322.5	751	324.0	754
325.5	754	327.0	751	328.5	754	330.0	754	334.5	754	333.0	754
334.5	754	336.9	254	337.5	754	339.8	754	346.5	754	342.0	754
343.5	754	345.8	754	346.5	754	348.0	754	349.5	754	354.2	751
352.5	754	354.0	751	355.5	751	357.8	754	358.5	754	340.6	751
364.5	751	363.9	754	364.5	754	366.0	754	367.5	751	369.8	/54
370.5	754	372.0	754	373.5	754	375.0	754	376.5	754	378.0	75.1
379.5	754	384.0	754	392.5	754	384.9	754	385.5	754	387.9	754
388.5	751	390.0	751	394.5	751	393.6	75.4	394.5	75 f	396.8 405.0	754 754
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415.5	733	417.8	725	448.5	7.58	428.8	718	421.5	787	423.0	698
424.5	696	426.0	686	427.5	683	429.0	674	430.5	868	432.6	661
433.5	657	435.0	653	436.5	649	438.0	644	439.5	637	441.8	633
442.5	628	444.0	621	445.5	619	447.8	613	448.5	668	456.6	893
454.5	694	493.8	596	454.5	592	456.0	587	457.5	586	459.8	584
460.5	588	462.0	574	463.5	572	465.6	565	466.5	561	468.6	557
469.5	853	474.9	553	4/2.5	545	4/4.8	541	475.5	53 <i>7</i>	477.0	533
478.5	529	480.6	525	481.5	522	483.0	5 19	484.5	543	486.6	5 18
487.5	587	489.8	504	498.5	478	492.0	496	493.8	492	495.0	487
496.5	484	498.0	4/7	499.5	474	584.8	4/2	502.5	469	504.6	465
505.5	464	507.0	468	508.5	455	510.0	453	511.5	452	543.0	459
514.5	447	546.8	442	547.5	441	549.8	439	520.5	434	522.0	438
523.5	427	525.0	425	526.5	422	528.0	417	529.5	448	531.8	448
532.5	488	534.0	465	535.5	464	537.8	462 387	538.5	466 385	54 0.8 549.0	396 384
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2944.5	3 2946.0	3 2947.5	2 2949.0	2 2950.5	2 2952.0	S
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37.5	4	39.0	4	40.5	. 4	42.0	ક	43.5	6	45.0	9
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82.5	62	84.0	61	85.5	61	78.0 87.0	54 61	79.5 88.5	63 66	84.0 90.0	63 58
91.5	58	93.0	58	94.5	57	96.0	57	97.5	56	99.8	55
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427.5	30	129.8	29	130.5	29	432.0	53	133.5	23	135.0	29
136.5	29	138.0	29	139.5	38	141.6	38	442.5	30	144.8	38
145.5	30	147.8	30	448.5	39	150.0	39	151.5	30	453.0	30
154.5	29	156.8	29	157.5	28	159.0	27	168.5	26	162.0	25
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247.5	11	249.0	11	220.5	11	222.8	10	223.5	18	225.0	19
226.5	18	228.0	10	229.5	9	231.6	9	232.5	9	234.8	9
235.5	9	237.9	9	238.5	8	240.0	3	241.5	8	243.0	8
244.5	8	246.8	7	247.5	7	249.0	7	250.5	7	252.0	7
253.5	7	255.9	7	256.5	7	258.0	7	259.5	7	264.9	7
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346.5	Š	348.0	š	319.5	š	321.6	š	322.5	Š	324.6	5
388.8	5	327.0	5	328.5	ŝ	330.0	š	331.5	š	333.0	š
334.5	5	336.0	5	337.5	5	339.6	ŝ	348.5	ŝ	342.0	4
343.5	4	345.0	4	346.5	4	348.9	4	349.5	4	354.0	4
352.5	4	354.0	4	355.5	4	357.6	4	358.5	4	368.6	4
364.5	4	363.0	4	364.5	4	366.0	4	367.5	4	369.0	4
370.5	4	372.0	3	373.5	3	375.0	3	376.5	3	378.0	3
3795 3885	3 3	384.0 390.0	3 3	382.5 394.5	3	384.0	3	385.5	3	387.0	3
397.5	3	379.8	3	400.5	3	393.0 402.6	3 3	394.5 403.5	3	396.0 465.0	3 3
406.5	3	488.0	3	469.5	3	411.0	3	412.5	3	414.6	3
445.5	3	417.8	3	418.5	$\ddot{3}$	420.0	ă	424.5	3	423.8	3
424.5	3	426.0	3	427.5	ž	429.0	ž	438.5	ä	432.6	ä
433.5	S	435.8	S	436-5	2	438.0	3.	437.5	ş	441.8	2
442.5	2:	444.8	2	445.5	2	447.6	2	448.5	2	456.0	2
451.5	S	453.9	S	454.5	S	456.0	5	457.5	8	459.0	2
460.5	7	462.8	2	463.5	2	465.6	2	466.5	2:	468.0	S S
469.5	5	4/1.8	S	472.5	2	474.8	S	475.5	s	477.0	S
478.5 487.5	2!	480.0	5	481.5	2	483.8	2	484.5	2	486.6	2 2 2
496.5	2	489.0 498.0	2 2	498.5 499.5	5	492.8	5	493.5	5	495.0	2
505.5	S	507.0	S	499.5 568.5	S	501.0 510.8	5 5	562.5 511.5	5	564.9	ر ا
514.5	2	546.6	2	547.5	2	519.0	2	520.5	2	543.0 522.0	2
623.5	Ş	525.0	ŝ	526.5	ş	233.8	2	529.5	Ş	531.8	2 2 2 2
532.5	2	534.6	ž	535.5	ž	537.0	ž	538.5	2	546.0	2
544.5	Š	543.0	Š	544.5	ŝ	546.0	4	547.5	1	549.8	4
550.5	1	552.0	4	553.5	4	555.0	2	556.5	ż	558.0	4
559.5	4	564.8	4	8.562	4	564.0	4	565.5	4	567.0	4

	568.5	4	579.8	4			573.0		(****		r: 77 / /3	
		1		1	571.5	4		1	574.5	4	574.0	1
4	5 77.5	1	579.0	1		1		1	583.5	- 1	585.0	4
	586.5	1	588.0	1	589.5	1	594.0	4	59 2.5	4	594.8	4
	59 5.5	1	597.0	4	598.5	4	666.6	4	681.5	4	603.0	4
)	504.5	4	696.8	4	607.5	Ä	309.0	4	640.5	i	612.8	ż
•		-		•		1				1		1
	613.5	1	615.0	1	616.5	1	648.0	1	619.5	1	624.6	1
	622.5	4	624.9	1	625.5	4	627.0	4	628.5	4	630.0	- 1
ľ	631.5	4	633.0	4	634.5	4	636.8	1	637.5	4	639.0	4
	649.5	Ā	642.8	4	643.5	•		4	646.5	- 4	648.8	i
		7		•		•		-		-		3
	649.5	1	651.0	1		1	654.6	1	6 55.5	- 1	657.0	1
	658.5	4	658.8	4	661.5	1	663.0	4	664.5	4	366.0	1
	667.5	1	669.0	4	670.5	4	672.0	4	673.5	1	675.0	4
	676.5	4	678.0	4	577.5	4	534.0	4	688.5	4	684.0	, i
		7		-		-				-		7
•	68 5.5	1	687 .0	1		- 1		4		1	693.6	1
	694.5	4	696.0	4	697.5	4	399.8	- 4	7 00. 5	- 1	702.0	4
	70 3.5	1	705.0	4	706.5	1	768.8	4	709.5	4	744.6	4
1	742.5	4	714.8	4	745.5	4	717.0	4	748.5	4	779.8	i
		•				•		•		-		1
	721.5	1	723.0	1	724.5	1	726.0	1	727.8	1	729.0	1
	730.5	1	732.8	4	733.5	- 1	735.4	- 1	736.5	4	738.0	1
	739 _* 5	1	741.0	1	742.5	4	744.0	1	745.5	4	747.8	4
	748.5	4	750.0	4	754.5	4	753.0	4	754.5	4	756.8	4
		4	759.0	•		•		4				
	757.5	-		•	766.5	1	762.0	•	763.5	1	765.0	7
•	766.5	1	768.0	1	769.5	4	774.0	4	772.5	4	774.8	- 1
	775.5	1	777.0	1	778.5	1	788.0	1	784.5	1	783.6	1
	784.5	4	786.0	4	787.5	4	789.0	4	798.5	4	792.8	4
1	793.5	4	795.0	1	796.5	4	798.0	4	799.5	4	801.0	
•		_						,				7
	802.5	1	304.0	1	805.5	1	897.9	1	8 88. 5	4	840.0	1
_	844.5	1	843.6	1	814.5	1	846.6	1	847.5	1	819.0	1
)	820.5	4	822.8	- 1	823.5	4	825 .0	4	826.5	- 1	828.8	4
	829.5	4	831.0	1	832.5	4	834.0	4	835.5	4	837.0	4
								- ;				
	838.5	4	849.9	1	844.5	4	843.0	7	844.5	1	846.0	1
•	847.5	1	849.0	1	850.5	1	852.0	- 1	853.5	- 1	855.0	1
	856.5	4	858.0	- 4	857.5	1	861.8	- 1	862.5	4	864.8	4
	865.5	4	867.0	1	868.5	4	828.0	4	874.5	4	873.6	4
•	874.5	•	876.0	•	877.5	•	879.8	•	880.5	- 1	892.8	
•				-		-		1				1
	88 3.5	1	885.0	1	886.5	1	888.0	1	889.5	1	891.0	1
	892.5	4	894.8	4	895.5	1	897.0	4	898.5	4	900.0	4
•	901.5	1	903.0	4	984.5	4	906.0	- 1	907.5	4	907.0	4
	949.5	4	942.8	4	943.5	4	945.0	4	946.5	4	948.0	4
	919.5	•	921.0	-		•	924.0	- 1	925.5	4	927.6	
				1	922.5	4				1		
•	928.5	1	930.0	4	934.5	1	933.0	1	934.5	1	936.8	1
	937.5	4	939.8	- 4	946.5	4	942.0	- 1	943.5	- 1	945.8	1
	946.5	4	948.0	4	949.5	4	954.0	4	982.5	4	954.0	4
•	955.5	4	957.0	4	958.5	4	960.0	4	961.5	4	963.0	4
		-		•		•		- 1		•	972.0	
	964.5	1	966.8	1	967.5	- 1	959.0	1	979.5	1		7
	973.5	1	975.0	4	976.5	4	978.0	1	979.5	1	984.6	1
	782.5	4	984.0	4	985.5	1	987 .0	1	988.5	1	990.8	4
	991.5	1	993.0	4	994.5	1	996.6	4	997.5	4	999.0	4
	1000.5	4	1002.0	4	1003.5		1885.8	4	1006.5	4	1668.9	1
	1969.5	- 1	1011.0		1612.5	1	1014.0	- 1	1015.5	1	1617.6	4
	1918.5	4	1020.0	4	1021.5	4	1923.8	4	4024.5	4	1026.0	4
	1027.5	4	1629.0	4	1638.5	4	1832.0	4	1033.5	4	1035.0	4
	1036.5	4	1038.0	-	1039.5	-	1841.9	4	1842.5	4	1844.8	4
												4
	1845.5	1	1047.6		1648.5	1	1050.6	1	1051.5	4	1053.0	
	1954.5	1	1856.8	1	1857.5	1	1859.0	1	1060.5	- 1	1862.8	4
	1063.5	4	1065.0	1	1066.5	1	1068.9	4	1069.5	4	1971.0	1
	1072.5	4	1074.0	4	10/5.5	-	1977.9	4	1078.5	4	1680.0	4
	1081.5	•	1083.0	•	1084.5		1086.6	4	1887.5	4	1909.6	4
		1								_		
	1090.5	- 1	1072.0		1093.5		1895.0	1	1896.5	1	1698.8	4
	1899.5	1	1101.0		1102.5	-	1164.6	1	1185.5	1	4492.0	8
	1468.5	Ø	1110.0	Ø	1111.5	Ø	4443.0	4	1414.5	4	1116.8	4
	1117.5	4	1119.0	4	1120.5	4	1122.0	4	1123.5	4	1125.6	4
	1126.5	4			1129.5		1131.0	- 4	1432.5	i	1134.0	i
		_										
	1135.5	1	1137.0	1	1138.5	1	1148.6	1	1141.5	1	1143.8	1

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1144.5		1 1146.0	6	1447.5	ü	1149.0	£.	1150.5	6	1452.0	0
1483.5		1455.0		1156.5		1158.0		1159.5		1106.0 1464.0	
1162.5		1 1164.0		1165.5		1 1167 6		1 1168.5		1170.0	
1171.5		14/3.0		11/4.5		1176.8		1177.5		11/9.8	
1180.5		1482.0		1183.5		4485.0		1186.5		1188.0	
1489.5		1494.0		1192.5		1194.6		1195.5		1197.0	
1198.5		1200.0		1201.5		1203.0		1204.5		1286.6	
1297.5		1207.0		1218.5		1242.0		1243.5	1	1245.0	
1216.5		1218.0		1219.5		1224.0		1222.5			
1225.5		1227.0		1228.5		1230.0		1231.5		1224.6	
1234.5		1236.0		1237.5		1239.6	1	1248.5		1233.0 1242.0	
1243.5		1245.8		1246.5		1248.0		1249.5		1251.8	
1252.5		1254.0		1255.5		1257.8					
1261.5		1233.0		1264.5		1266.0		1258.5		1260.6	
1270.5		1272.0		1273.5				1267.5		1269.0	
1279.5		1281.8		1282.5		1225.0 1284.0		1276.5		1278.0	
1288.5		1298.8		1291.5				1285.5		1287.0	0
1297.5		1279.8		1300,5		1293.0		1294.5		1296.8	8
1306.5		1388.0	1	1309.5		4302.0		1303.5		1385.9	8
1315.5		1347.8	7	1348.5		1311.0		1312.5		1314.8	1
1324.5		1326.0				4320.0		1321.5		1323.8	9
1333.5		1335.9		1327.5 1336.5		1329.6		1338.5		1332.6	9
1342.5		1344.8	87	1345.5	89	1338.0		1339.5		1344.8	4
1354.5						1347.8		1348.5		1356.6	6
1360.5		4353.0 4362.0		1354.5 1363.5		4356.0		1357.5		1359.8	9
1369.5		1302.0		1303.5		1365.6		1366.5		1368.8	Ю
1378,5		1380.0		1376.5		1374.9		1375.5		4377.8	0
1387.5		1389.8		1370.5		1383.8		1384.5		1386.0	1
1396.5		1398.0		1378.5		1392.0		1393.5		1395.8	1
1405.5		1407.0		1468.5		1481.6		1462.5		1484.8	1
1414.5		1416.8				1410.0		1411.5		1413.0	4
1423.5				1417.5		1419.0		1428.5		1422.0	9
1432.5		1425.0		1426.5		4428.8		1429.5		1431.8	8
		1434.0		1435.5		1437.0		1438.5		1448.8	4
1441.5 14 50 .5		1443.0 1452.0		1444.5		1446-8		1447.5		1449.0	1
1459.5				1453.5		1455.0		1456.5		1458.6	8
1468.5		1461.0		1462.5		1464.8		1465.5		1467.8	9
1477.5		1470.0 1479.0		1471.5 1480.5		1473.0		1474.5		1476.6	4
1486.5		1428.0				1482.0		1483.5		1485.9	4
1495.5		1497.8		1489.5		1491.0		1492.5		1494.8	4
1504.5		1506.0		1498.5		4500.0		1501.5		1503.0	4
1513.5		1515.0		1507.5		1569.6		1510.5		1512.0	4
1522.5		1524.8		1516.5	1			1519.5		1521.0	4
1534.5		1527.0		1525.5	1	1527.6		1528.5		1530.8	9
1540.5		1542.0		4534.S		4536.0		1537.5		1539.0	9
1549.5		1551.0		4543.5 4552.5		1545.0	81	4546.5		1548.0	9
1558.5	_	1560.0				1554.0		1555.5		1557.0	
1567.5	(A)		9	1561.5	9	4563.0		1564.5	9	1566.0	0
1576.5	8	1569.8		1570.5		4572.0		1573.5	8		9
1585.5	Ø	1578.0 4607.0		1579.5	8	1581.0	6	4582.5	8		6
1594.5	4	1587 - 0		1588.5		1590.0		1591.5	8		4
1603.5		1596.0 1605.0	4	4597.5				1666.5		1682.8	0
1642.5	1			1686.5		1698.9	•	1609.5	1		4
				1615.5		1617.0	4	1618.5	1	1628.8	4
1621.5 1630.5		4623.8		1624.5		1626.8	_	1627.5		1629.8	9
		1632.0		1633.5		1635.0	9	1636.5		1638.0	Ø
1639.5 1 64 8.5	_	1641.9	8			1644.8	4		1		8
1657.5	9	1650.0	9	1651.5		1653.0	0	1654.5		1656.0	9
105/.5 1666.5		1659.0	_	1660.5		1662.8		1663.5		1665.0	9
1675.5	E 3	1668-8	/da	1669.5		1671.8	6	1672.5	21		37
10/3.8 1684.5		1677.0		1678.5		1689.8		1681.5		1683.9	133
1693.5	141	1686.0 1695.0	147	1687.5 1696.5		1689.9		1498.5		1692.0	448
17 0 2.5						1698.0		1699.5		4784.8	45
4744.5		1794.0		4705.5		4707.0		4208.5		17 10 . 6	53
7/ 77.0	() T	1713.0	07	1714.5	77	1716.0	ชธ	4747.5	86	1719.8	97

_	1729.5		4722.0		4723.5	188	1725.0		4726.5		4728.8	168
•	1729.5		4734.8		1732.5		1734.0		4735.5		1737.6	85
	1738.5		1748.8		4744.5		1743.0	64	1744.5		1746.0	54
,	1747.5		1749.8		4750.5		1252.6	38	4753.5		4755.6	37
•	1756.5 1765.5		1758.8 1767.8		4759.5 4768.5		1764.0 1770.0	29	4762.5	47	1764.0 1773.0	26 14
	1/74.5		1776.0		1777.5		1779.8		1/30.5		1782.8	8
	1783.5		4785.0		1786.5		1788.8		1789.5		1791.6	5
	1792.5		1794.8		1795.5		1797.0	4	1798.5		1888.8	ä
	1801.5		4863.0	3	1884.5	3	1806.8	2	4887,5	2	1889.0	2
•	1819.5	S	4842.8	2	1813.5		1815.0	8	1816.5		1818.9	2
	1819.5		1821.0		1822.5		1824.6		4825.5		1827.0	2
_	1828.5		1830.0		1831.5		1833.0	•••	1834.5		1836.8	9
•	1837.5		1839.0		1848.5		1842.6		4843.5		1845.8	43
	1845.5		4848.8		1849.5	44	1851.0	14	4852.5		1854.8	15
•	1855.5 1844.5		1857.0 1866.0		1858.5 1867.5		1866.0 1869.0		1861.5 187 8. 5		1863.8 1872.8	14 9
_	1873.5		1875.0		1876.5		18/8.8		18/9.5		1881.8	4
	1882.5	-	1884.0		1885.5		1887.8		1888.5		1879.8	2
•	1891.5		1873.0		1894.5		1896.8	4	1897.5		1899.6	4
	1900.5		4902.0	4	1903.5		1905.0	4	1986.5		1788.9	4
_	1989.5		1911.6	2	1912.5	2	1914.8	2	4945.5	2	1917.0	5
•	4948.5		1929.9		1924.5		1923.0		1924.5		1926.8	3
	1927.5		1929.0		1930.5		1932.0		1933.5		1935.8	3
•	1936-5		4938.0		1939.5		1944.8		4942.5		1944.8	2
•	1945.5		4947.8		1948.5		1958.6		1951.5 1960.5		1953.6 1962.6	4
	1954.5 1963.5		1956.0 1965.0		1957.5 1966.5		1959.0 1968.0	4	1700.5		1902.0	4
•	1972.5		19/4.8		1975.5		1977.0		1978.5		1580.0	4
-	1981.5		1983.0		1984.5		1986.0		1987.5		1989.8	4
	1990.5		4992.8		1993.5	4	1995.0		1996.5		1998.8	4
	1999.5	4	2001.0	4	2002.5	4	2004.0	4	2005.5	4	2897.6	4
	2008.5		2949.9	1		4	2043.0	4		1	8.6185	1
_	2047.5		2649.6		2020.5	4			2023.5	1	2025.6	4
•	2026.5		2028.0	4	-,		2834.6	1			2034.0	•
	2035.8		2037.6	1			2046.6		2841.5			1
•	2 044. 5 2 0 53.5	1	2046.0 2055.0	1	2056.5	1		1	2059.5 2059.5		2052.0 2064.0	4
•	2062.5		2864.8	•	2045.5	4		-	2068.5		2070.0	4
	2871.5		2073.0	4		•	20/6.8	4	2077.5	4	20/9.6	4
•	2089.5	-	2082.0	•	2083.5	4		-	2686.5		86883.8	4
	2089.5	4	2094.0		2092.5	4	2074.6	4	2898.5	1	2097.6	4
_	2098.5	4	8.8018	1		1	2103.8	1	2404.5	4	2486.8	4
	2187.5	1			2418.5		2112.0		2443.5		2115.6	•
	2116.5	4	2448.0	1	2419.5		2424.0	4	2422.5	•	2424.8	4
•	2425.5		2127.0		2428.5		2130.0		2434.5 2448.5		2433.0 2442.8	4
•	2134.5 2143.5		2436.8 2445.0	-	2437.5 2446.5		2439.8 2448.0		2149.5		2454.0	4
	2152.5	-	2454.8		2455.5		2467.8		2458.5		2169.9	4
•	2161.5		2163.0		2164.5		2166.6	4			2169.6	4
	2470.5		2472.0		2473.5		2175.8		24/6.5		2478.8	4
	2179.5		2181.0		2482.5		2184.8		2485.5		2487.0	4
•	2488.5		2490.0		2494.5		2193.0	1			2496.0	8
	2197.5		2499.0		2200.5		2202.0		2203.5		2205.0	В
	8804.2		2208.0		2289.5		2244.0		8.5155		8.4455	8
ļ	2245.5		2247.8	-	2248.5		2220.0		2221.5		2223.6	4
	2224.5		2226.8		2227.5		2229.0		2239.5		2232.0 2244.6	8
	2233.5		2235.0 2244.0		2236.5 2245.5		2238.8 2247.8		2248.5		2258.8	8
	2242.5 2251.5		2253.0		2254.5		2256.0		2257.5		2259.8	8
	2268.5		5595*8		2263.5		2262.0		2244.5		2268.9	ä
	2269.5		2274.0		2272.5		2274.8		22/5.5		22/7.8	ä
	8878.5	9	8.8888		2284.5		8.6833		2284.5		8.6855	8
•	2287.5	8	2289.0		2290.5	0	2292.0	9	2293.5	8	2295.0	8

0 2298.0 2296.5 0 2299.5 8 2384.8 8 2382.5 0 2304.6 2305.5 0 2307.0 0 2368.5 8 2348.8 9 2311.5 8 2343.0 2314.5 0 2349.0 0 2320.5 0 2346.0 4 2347.5 0 2322.6 2323.5 2325.0 2325.5 S358*8 8 2327.5 9 2334.9 2332.5 0 2334.0 0 2335.5 0 2337.0 0 2338.5 0 2346.9 2344.5 2343.0 8 2344.5 8 2346.8 2347.5 8.2349.8 0 2353.5 0 2355.0 0 2356.5 0 2358.8 2350.5 0 2352.0 0 2364.0 0 2365.5 8 2367.8 2359.5 Ø 2364.8 0 2362.5 0 2376.0 2368.5 8 2378.8 8 2374.5 0 2373.0 0 2374.5 0 2379.0 9 2380.5 8 8382.8 0 2303.5 8 2385 8 23/7.5 2386.5 0 2391.6 8 2392.5 0 2388.0 0 2389.5 8 2394.6 0 2486.0 9 2494.5 9 2483.8 2395.5 0 2397.0 8 2398.5 Ø 0 2469,0 8 2448.5 0 2412.0 2484.5 Ø 2496.8 0 2467.5 2443.5 2445.8 8 2446.5 0 2448.0 9 2419.5 8 2424.8 и u 2422.5 2424.0 2425.5 9 2427.8 0 2428.5 8 2438.8 9 2437.5 2434.5 9 2434.5 8 2436.8 0 2439.0 ø 0 2433.0 2449.5 0 2443.5 0 2445.6 0 2446.5 8 2448.8 2442.8 И 9 2457.0 0 2454.0 2449.5 9 2454.0 8 2455.5 8 8 2462.5 2458.5 8 2468.8 0 2463.6 0 2461.5 0 2464.5 9 2466.9 н 9 2472.9 2469.8 8 2478.S 0 24/3.5 9 2475.9 а 2467.5 Ø 2476.5 Ø 2478.0 0 2479.5 0 2484.6 6 2482.5 0 2484.6 H 2490.0 2494.5 8 2493.9 2485.5 ø 2487.9 Ø 2488.5 Ø Ø H 2459.0 2494.5 9 2496.8 0 2497.5 8 9 2599.5 0 2502.0 ø 2503.5 2585.0 2596.5 0 8508.0 9 2509.5 9 2544.8 B 2512.5 0 2514.0 0 2545.5 0 2547,0 0 2548.5 8 2528.6 Ø 2824.5 0 2523.0 0 2524.5 9 5556.0 0 2527.5 9 S255°9 ø 2530.5 8 2532.8 0 2533.5 0 2535.0 9 2836.5 0 2538.6 6 2539.5 8 2544.0 0.2542.5 0 2544.0 8 2845.5 9 2547.9 Ø 0 2554.5 0 2554.5 2548.5 0 2550.6 0 2553.0 0 2556.6 Ø 2557.5 8 2559.8 8 2560.5 0 2562.0 8 8563.5 9 2565.0 0 0 2574.0 0 2574.6 6 2572.5 2566.5 0 2568.0 0 2569.5 A 2575.5 0 2577.0 8 2578.5 8.08838 9 2584.5 9 2593.8 0 2589.0 0 2586.0 0 2587.5 0 2590.5 0 2592.0 2584.5 K 2593.5 2595.0 6 2598.8 8 2599.5 Ø 8 2576.5 0 2504.0 ð 2602.5 2684.6 0 2687.0 9 2688.5 H 0 2605.5 8 2618.0 в 2646.8 9 2647.5 9 2619.9 Ð 2644.5 0 2643.0 8 2614.5 2620.5 0 2622.0 0 2623.5 0 2625.0 0 2626.5 0 2628.0 H g Ø 2629.5 9 2634.9 8 2632.5 9 2634.0 2635.5 0 2637.0 2638.5 0 2640.0 8 2641.5 Ø 2643.0 Й 2644.5 Ø 2646.8 H 2647.5 2659.5 2649.0 2652.0 8 2653.5 0 2455.9 ø я Ø 8 2656.5 Ø 2658.0 0 2659.5 и 2661.8 Й 2662.5 2664.6 2665.5 0 2667.8 Ø 2668-5 Ŋ 2670.9 8 2674.5 0 2673.0 a 2679.8 2674.5 a 2676.0 0 2677.5 Ø 8 2680.5 6 2682.6 6 2685.0 9 2688.9 0 2694.0 2683.5 2486.5 0 2689.5 ð Й ü 2766.6 В 2692.5 8 2694.0 8 2695.5 8 2697.0 0 2698.5 В 2784.5 2703.0 9 2/99.9 Я 2791.5 Я Я 8.286.8 9 2797.5 2710.5 0 2712.0 Ø 2743.5 8 2745.6 8 2746.5 B 2748.6 B 8 2/24.8 2719.5 2724.0 8 2725.5 0 2727.8 2722.5 ø H 0 2728.5 2730.0 2731.5 2733.0 2734.5 0 2736.6 8 2748.8 2739.0 0 2743.5 9 2745.0 2737.5 Ø 8 2740.5 2748.0 2749.5 1 2754.6 0 2752.5 Ø 2254.6 ø 2746.5 Ø 8 8 8768.8 2785.5 2757.0 2758.5 0 2764.5 0 2763.9 ø H H 0 2767.5 2764.5 2766.0 8 2769.6 9 2770.5 0 2772.0 ø 2773.5 8 27/5.0 Ø 2776.5 8 2778.8 9 2779.5 8 2284.9 6 2788.5 2784.0 2785.5 2782.5 Ø 0 2787.0 8 2798.8 Й () 8/96.8 2797.5 8.4672 2794.5 2793.0 ø 2794.5 ij 0 d 8 2805.0 2800.5 2802.0 Ø 2803.5 Ø Ø 2806.5 2888.6 Ø Ø H 2889.5 2844.8 2842.5 ø 2844.8 8 2845.5 ø 2847.8 2823.8 28 18.5 2820.0 a 2824.5 0 ø 2824.5 8 2826.6 2827.5 2829.0 2838.5 Ø 2832.0 8 2833.5 H 2835.0 2841.8 2839.5 2842.5 2844.8 2838.0 Ĥ A A В 2836.5 2845.5 2848.5 2850.0 2854.5 2853.0 2847.0 2859.8 8 8 9 2868.5 Pi 2862.8 -R 2856.0 2857.5 2854.5 5.8983 8 2865.8 2866.5 8.888 2869.5 0 2874.0

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2872.5	0 2874.0	0 2875.5	9 2877.0	0 2878.5	8 2888.8	9
2881.5	0 2883.0	0 2884.5	0 2886.0	0 2887.5	0 2889.6	8
2890.5	0.2892.0	0 2893.5	9 2895.0	9 2896.5	0 2898.0	8
2899.5	0 2904.0	0 2902.5	0 2964.0	8 2985.5	0 2907.0	6
2908.5	8 2240.8	8 2911.5	8 2943.8	0 2914.5	8 2916.8	9
2942.5	8 2949.0	0 2920.5	9 2922.0	0 2923.5	0 2925.0	9
2926.5	9 2928.9	0 2929.5	0 2934.0	6 2932.5	9 2934.0	9
2935.5	0 2937.0	0 2938.5	0 2940.6	0 2944.5	0 2943.0	0
2944.5	9 2946.9	0 2947.5	0 2949.0	9 2959.5	0 2952.0	ø
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TABLE 3
1766.0 0.1629E-02 0.1344E 01
2650.0 0.4570E-02 0.4009E 04
   4.5 0.3949E-09 0.5879E-09
   3.9 0.2280E-08 0.4003E-08
   4.5 0.4810F-08 0.1122E-07
   5.9 0.6476E-98 0.2049E-07
   7.5 0.4202E-07 0.3852E-07
   9.0 0.4539E-07 0.6464E-07
  40.5 0.2328E-02 0.9653E-67
  12.0 8.4294E-07 8.1609E-06
  43.5 0.5243E-07 0.2396E-06
  45.9 0.6594E-07 0.338SE-06
  16.5 0.8622E-07 0.4678E-06
  48.0 0.4035E-05 0.6239E-06
  19.5 0.1254E-06 0.8111E-06
  24.0 0.4769E-06 0.4077E-65
  22.5 0.1937E-06 0.1367E-05
  24.0 0.2250E-06 0.4785E-05
  25.5 0.2626E-06 0.2098E-05
  27.0 0.3232E-06 0.2583E-05
  28.5 0.3966E-06 0.3478E-05
  39.9 0.4941E-96 0.3919E-05
  31.5 0.55282-06 0.47562-05
  33.0 0.64675-06 0.57265-05
  34.5 0.7068E-06 0.6786E-05
  36.0 0.7730E-96 0.7946E-85
  37.5 0.8907E-06 0.9282E-05
  39.8 0.9795E-96 0.497SE-04
  40.5 0.4678E-05 0.423/E-04
  42.0 9.1238E-05 0.1423E-04
  43.5 0.13238-05 0.16248-04
  45.8 8.1432E-85 8.1836E-84
  46.5 0.4552E-05 0.2069E-04
  48.8 0.1678E-05 0.2329E-04
  49.5 0.1843E-05 0.2597E-04
  51.9 0.1991E-05 0.2896E-04
  52.5 0.2139E-05 0.3216E-04
  54.0 0.2332E-95 0.3566E-04
  55.5 0.2593E-05 0.3955E-04
  57.0 0.2884E-05 0.4397E-04
  58.5 0.3489E-05 0.4866E-04
  60.0 0.3745E-95 0.S423E-04
  61.5 0.4243E-05 0.6059E-04
  63.0 0.4874E-95 0.6799E-04
  64.5 0.6054E-05 0.7698E-64
  66.0 0.7074E-05 0.8798E-04
  67.5 0.7986E-05 0.9956E-04
  69.0 0.9849E-95 0.1434E-83
  70.5 0.9748E-05 0.1278E-03
  72.0 9.4028E-94 0.4432E-03
  73.5 0.4874E-04 0.4592E-03
  75.0 0.4445E-94 0.4769E-03
  76.5 8.4468E-84 8.4934E-83
  78.0 0.4205E-94 0.2445E-03
  79.5 0.4253E-04 0.2383E-63
  84.0 0.4304E-04 0.2498E-03
  82.5 0.4350E-04 0.2700E-63
  84.0 9.4399E-04 0.2949E-03
  85.5 0.4450E-04 0.3428E-03
  87.8 0.4584E-94 0.3353E-93
  88.5 0.4553E-04 0.3586E-03
  90.0 9.460/E-04 0.382/E-03
  91.5 0.16646-04 0.46766-03
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